

NOVEL CERAMICS AND COMPOSITES PROCESSING TECHNOLOGIES FOR ENERGY-INTENSIVE APPLICATIONS

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MW-CVI production of large SiC-based CMCs for energy intensive industries: a challenge won?

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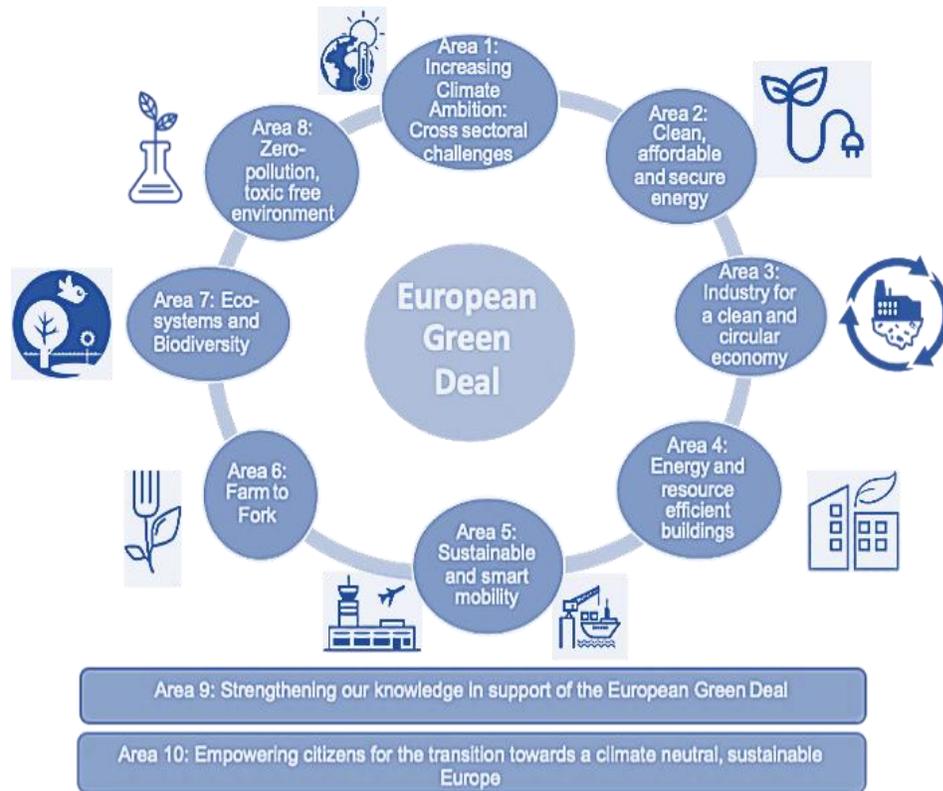
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Summary

- 1) Introduction
 - a) Energy-intensive industries & steelmaking decarbonization pathways;
 - b) CMCs application in steelmaking sector;
 - c) CMCs manufacturing methods;
- 2) MW-CVI process background
 - a) Design & Improvements of the MW-CVI pilot plant
 - b) Challenges and Upgrades
- 3) MW-CVI processing of large SiC-based CMCs
 - a) MW-CVI processing of SiC_f/SiC square-shaped preforms
 - b) MW-CVI processing of SiC_f/SiC tubular-shaped preforms
- 4) Conclusions

1. Introduction

- ❖ Over the last century an increasing need to develop stronger, tougher and more chemically resistant structural materials has been observed
- ❖ Steelmaking industries will need to follow one or more low carbon emissions pathways

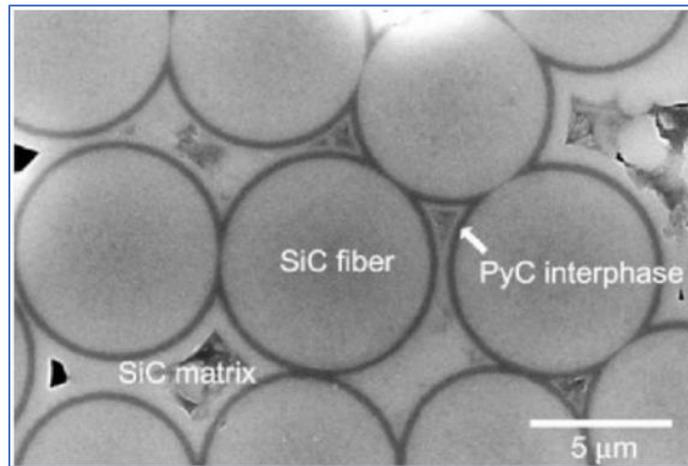


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https://automotive.arcelormittal.com/news_and_stories/blog/2019PathToLowCarbonSteelmaking

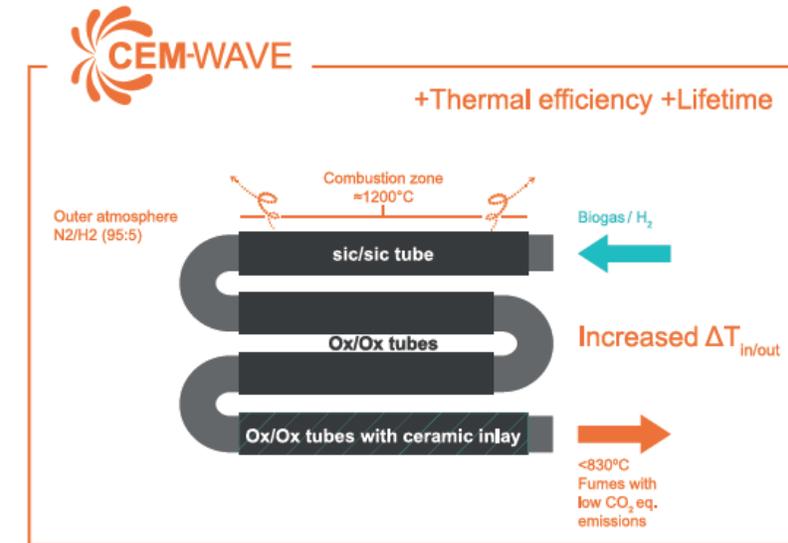
❖ **SiC_f/SiC CMCs** are promising materials for thermo-structural applications in various strategic sectors (i.e. aerospace, energy) due to their:

- Good high-temperature mechanical properties
- Low density
- High toughness
- High oxidation resistance



❖ In the framework of the **EU CEM-WAVE project**, the application of SiC_f/SiC has been proposed for the replacement of Inconel superalloys in the hottest section of *radiant tube furnaces* for steelmaking applications:

- T^{MAX} ~ 900-1000°C
- Average lifetime ~ 4 years

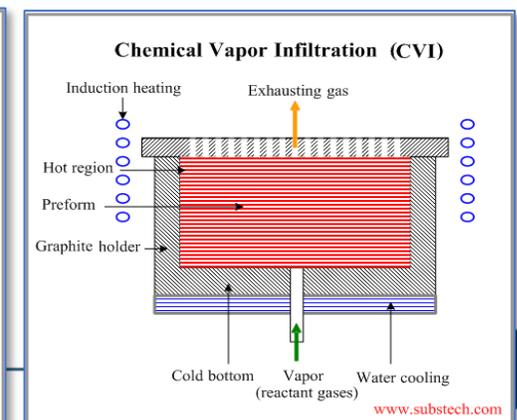
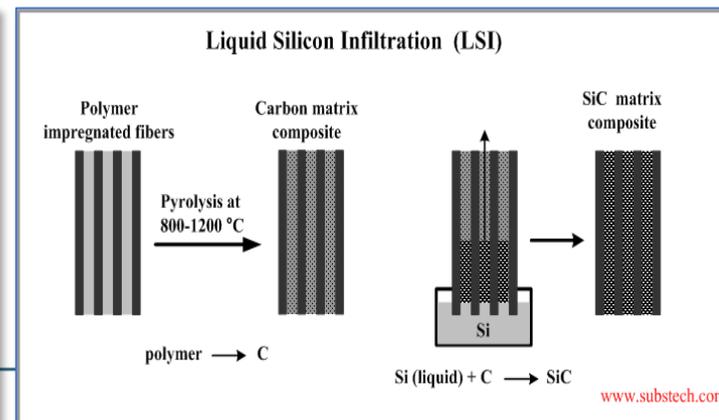
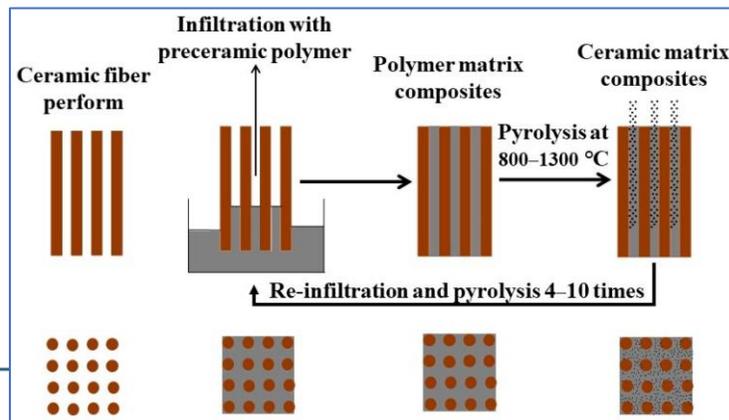


Simplified SiC matrix synthesis processes are needed to reduce production costs

Kim, Daejong & Kim, Weon-Ju & Park, Jeong Yoon. (2012). Compatibility of CVD SiC and SiCf/SiC Composites with High Temperature Helium Simulating Very High Temperature Gas-Cooled Reactor Coolant Chemistry

1.1 SiC_f/SiC CMCs manufacturing by infiltration methods

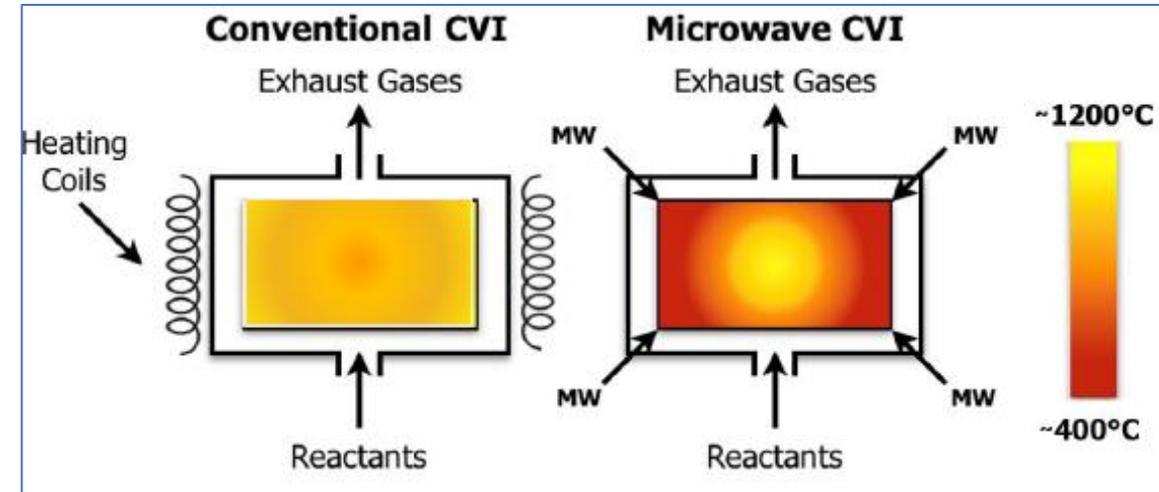
| | <u>Polymer Infiltration and Pyrolysis (PIP)</u> | <u>Liquid Silicon Infiltration (LSI)</u> | <u>Chemical Vapor Infiltration (CVI)</u> |
|----------------------|--|--|---|
| Advantages | <ul style="list-style-type: none"> Low temperature (prevents fiber damage) Good control of microstructure and composition No free silicon in the matrix | <ul style="list-style-type: none"> Low cost Short production time Low residual porosity | <ul style="list-style-type: none"> High purity matrices Low temperature (prevents fiber damage) Excellent mechanical properties Often smooth process surfaces |
| Disadvantages | <ul style="list-style-type: none"> Multiple infiltration-pyrolysis cycles High production cost High residual porosity Poorly SiOC, SiCN crystalline matrices | <ul style="list-style-type: none"> High temperature and highly corrosive metal melt (may damage fibers) Residual free silicon Low mechanical properties Rough surfaces need machining with diamond tools | <ul style="list-style-type: none"> Very slow process (~several weeks) High residual porosity (15-20%) due to crusting High capital and production costs |



1.2 MW-CVI process: Advances & challenges

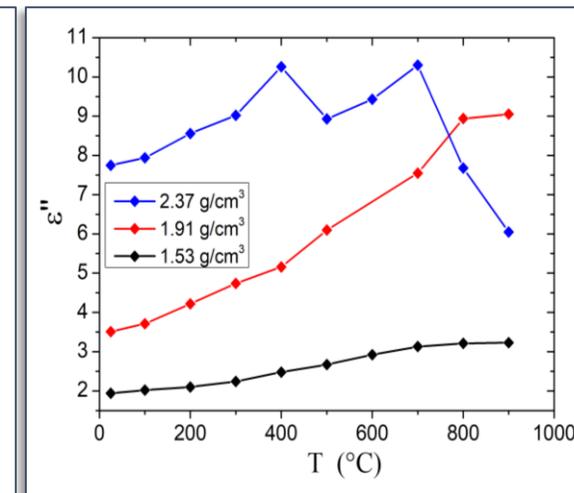
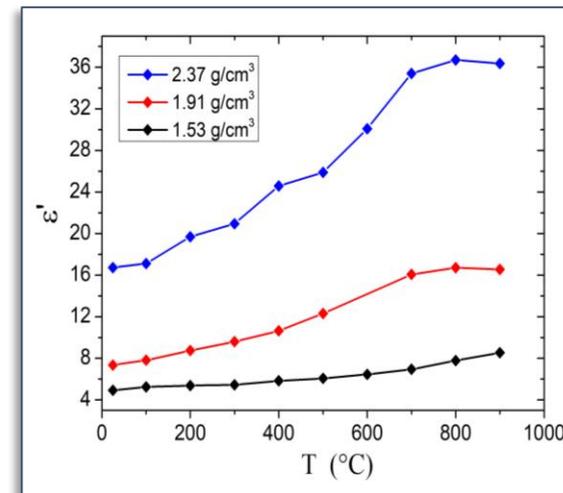
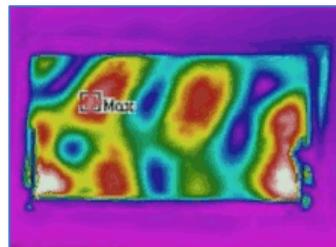
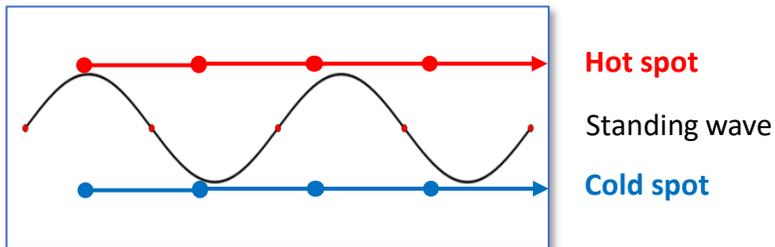
❖ The Microwave-assisted CVI (**MW-CVI**) is an attractive alternative to manufacture SiC-based CMCs due to:

- Sample volumetric heating (Inverse T profile)
- Faster processing
- Significant cost reduction



❖ Among the major challenges of MW-assisted processes there are:

- 1) Non-uniform heating
- 2) Plasma occurrence
- 3) Control and optimization of the MW-heating with dielectric properties change



D'Angi , A. "Microwave enhanced chemical vapour infiltration of silicon carbide fibre preforms." (2018).

2. MW-CVI reactor: Design & Improvements

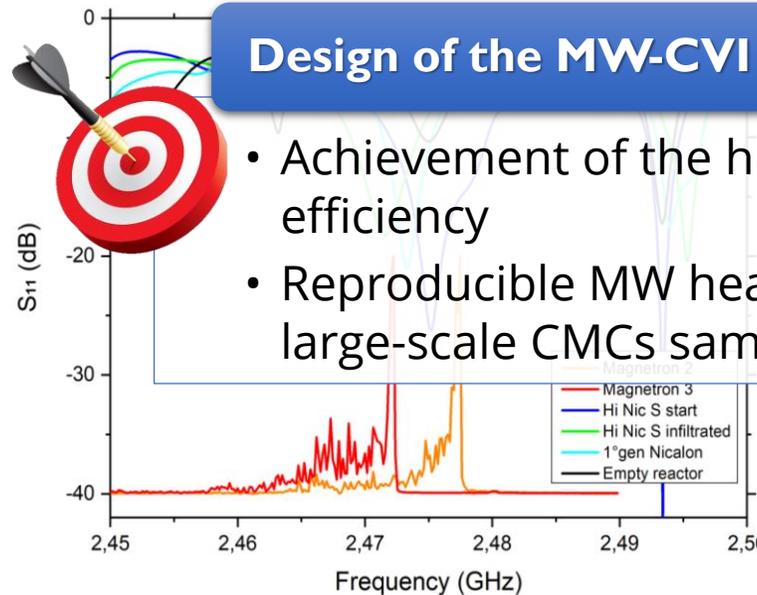


- **Duration:** 48 months (2012-06-01 to 2016-05-31)
- **Total cost:** EUR 10,285,626
- **EU contribution:** EUR 7,151,000
- **Programme acronym:** FP7-NMP
- **Subprogramme area:** NMP.2011.4.0-1
- **Contract type:** Large-scale integrating project



Design of the MW-CVI pilot plant in Pisa:

- Achievement of the highest MW heating efficiency
- Reproducible MW heating of relatively large-scale CMCs samples



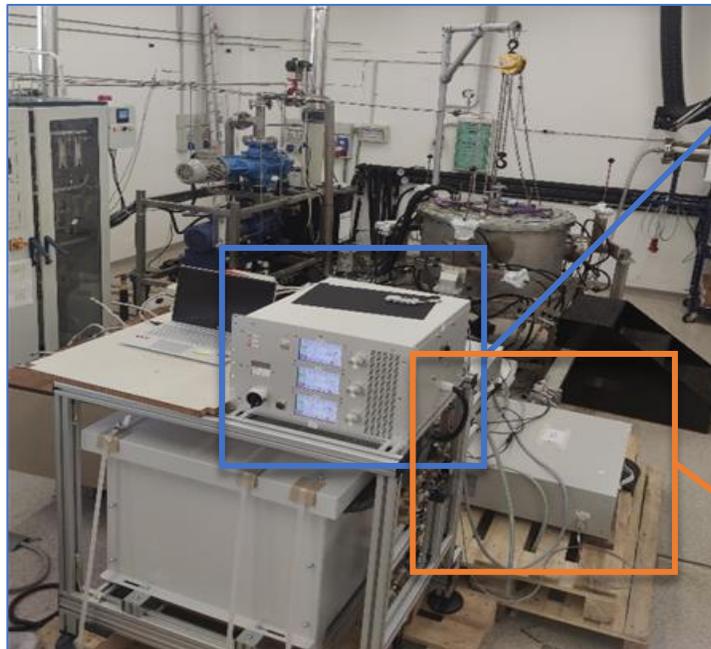
3 Magnetrons, each
frequency band 2,4 ÷

2,5 GHz

- 3 kW power

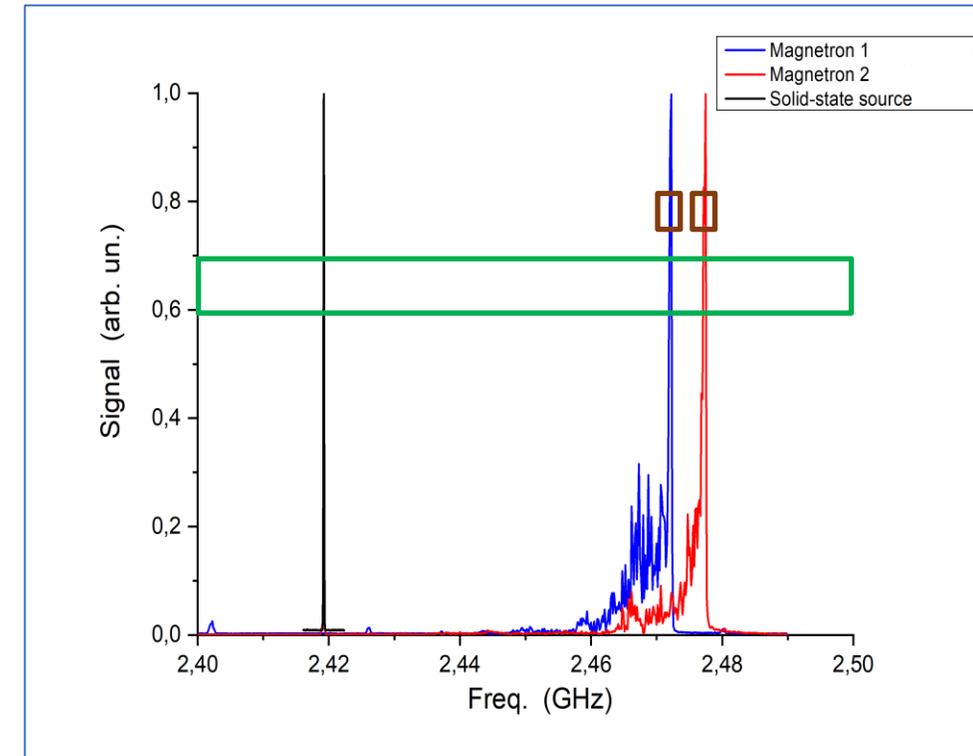
❖ A MW **Solid-State source** system has been developed by Fricke und Mallah (Peine, Germany):

- 3 x 2kW Solid-State Generators (SSGs)
- 2400 – 2500 MHz ISM band (1 MHz step)
- 3 x 3 kW isolator



Control unit interface

2 kW SSG + isolator



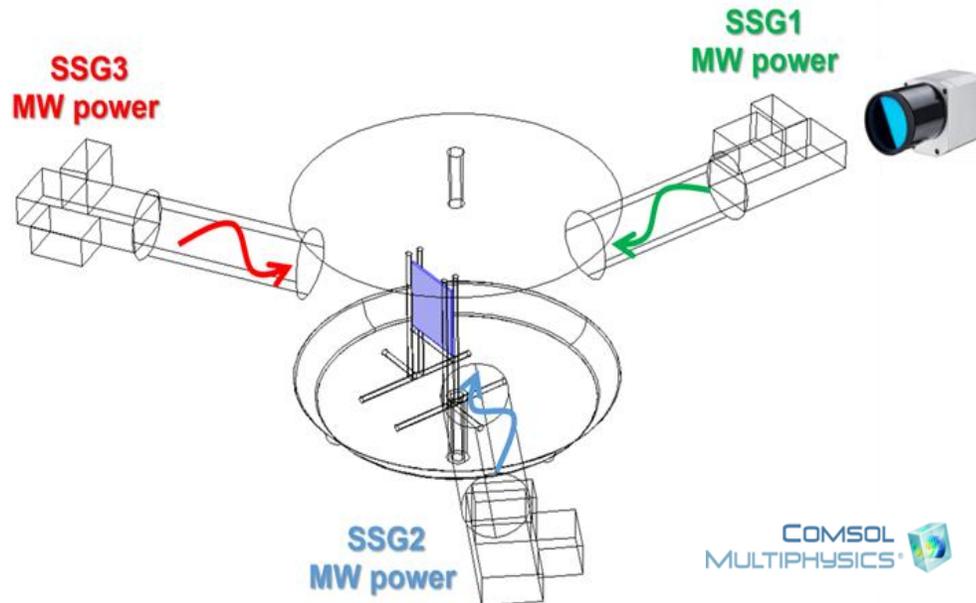
Design of a high quality **Overmoded** resonant cavity

Multiport excitation scheme



Optris PI 1M overview

| Temperature range | Spectral range | Frame rate | Detector |
|-------------------|----------------|-------------|--------------------------|
| 500 to 1800°C | 0,85-1,1 μm | Up to 1 kHz | CMOS, 764x480 px @ 32 Hz |



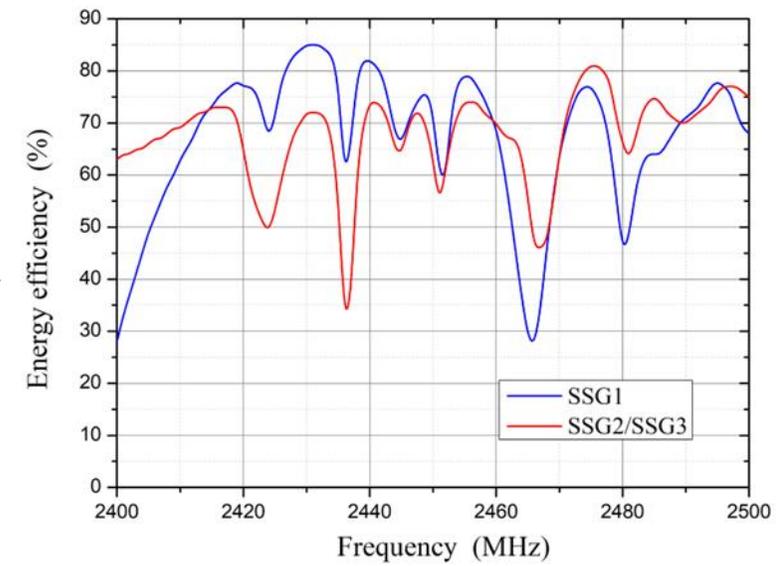
❖ A **Multiport-Multifrequency** approach has been developed, whose main benefits are:

- 1) Higher degree of electric field homogeneity;
- 2) Reduced risk of plasma formation;
- 3) Reduced risk of unwanted MW coupling between the different channels (cross-coupling) with higher process energy efficiencies;

Operating frequencies selection

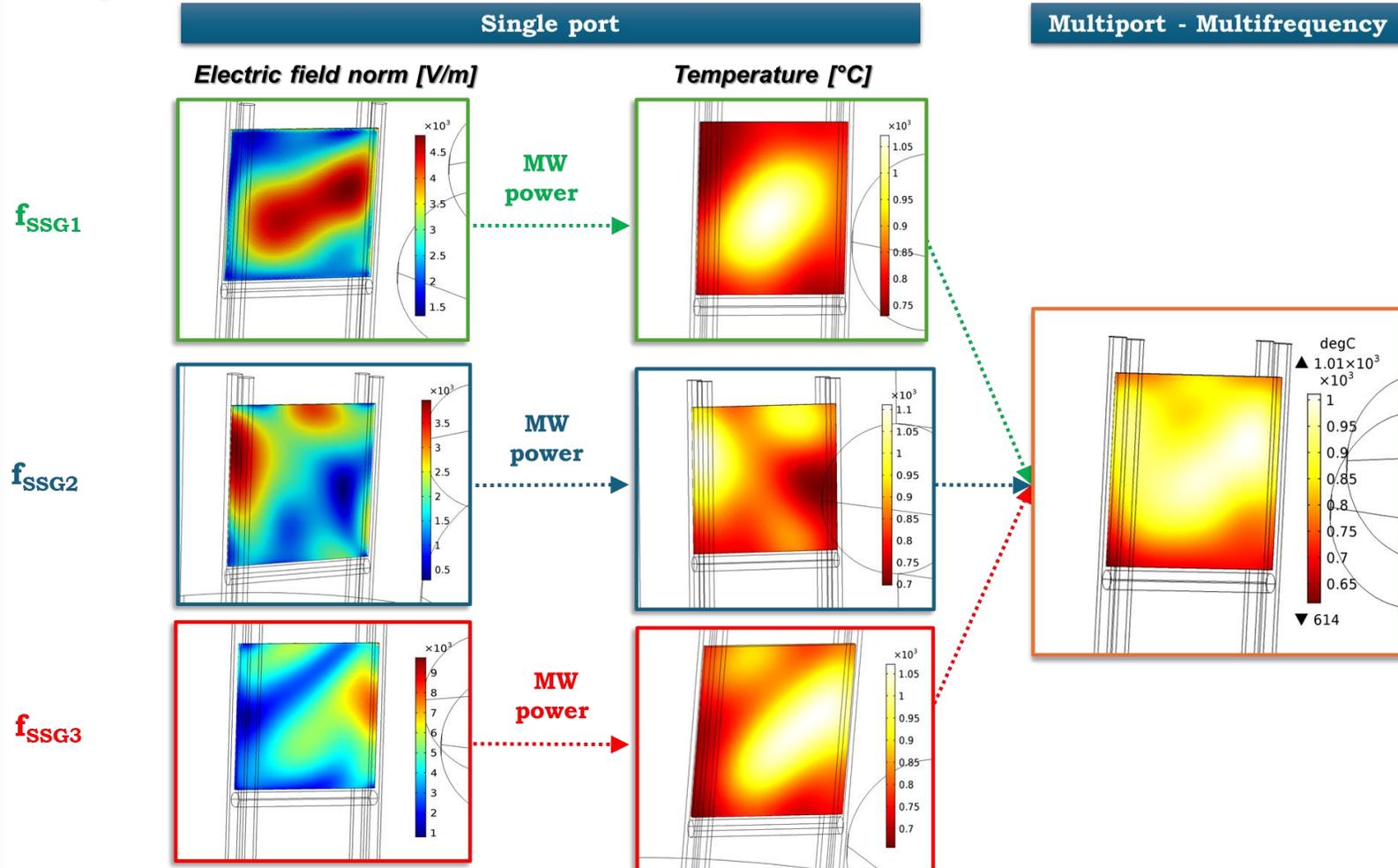
- Highest energy efficiency
- Mode characteristics
- Minimum cross-coupling

$$\eta = \frac{P_s}{P}$$



Single port

Multiport - Multifrequency



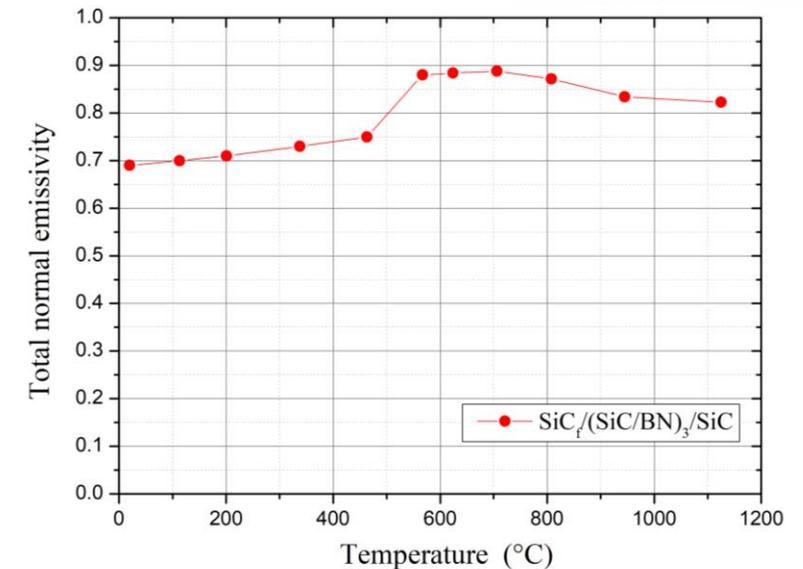
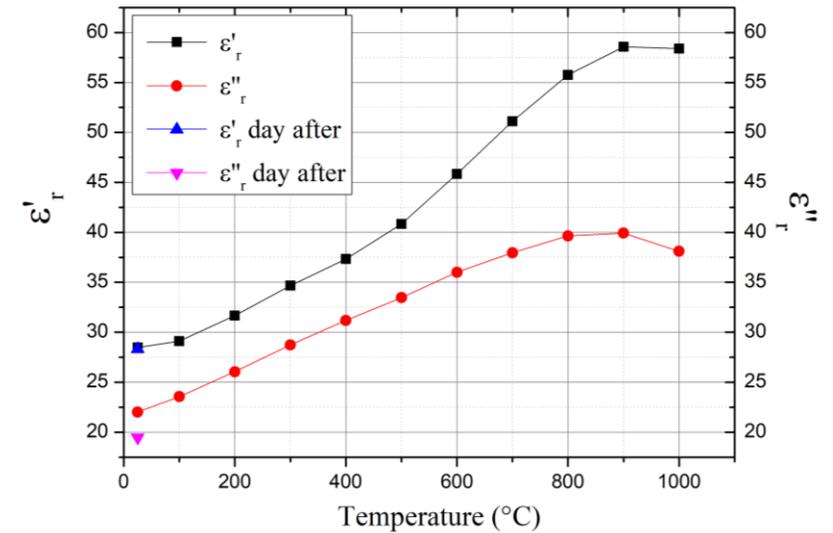
3. MW-CVI processing of large SiC-based CMCs

- ❑ Two square-shaped and one tubular-shaped $\text{SiC}_f/(\text{SiC}/\text{BN})_3/\text{SiC}$ preforms have been successfully infiltrated by the MW-CVI process;
 - The $\text{SiC}_f/(\text{SiC}/\text{BN})_3/\text{SiC}$ preforms have been manufactured by Filament Winding method by Fraunhofer ISC (Bayreuth, Germany)
- ❑ The Multiport-Multifrequency approach has been employed to tailor the SiC_f/SiC preforms temperature profile exploiting the frequency tunability of MW Solid-State sources;
- ❑ The choice of the most suited excitation frequencies has been guided by rigorous numerical modeling of the reactor loaded by the sample of interest;

| #ID sample | $\text{SiC}_f/\text{SiC}-1$ | $\text{SiC}_f/\text{SiC}-2$ |
|------------------------------------|-----------------------------|-----------------------------|
| Roving | 200 tex | 200 tex |
| Green body matrix | Epoxy | Epoxy |
| Pyrolised matrix | Carbon | Carbon |
| Porosity [%vol] | 40.0 | 40.0 |
| Density [g/cm^3] | 1.19 | 1.19 |
| Geometry [B x L x T, cm] | 10×10×0.26 | 10×10×0.27 |



- The dielectric properties have been determined as a function of the temperature up to 1000°C by a facility available at **IPCF-CNR** premises
- The total normal emissivity has been determined as a function of the temperature up to 1000°C by **CEMHTI** laboratory (Orléans - France)
- The SiC matrix densification pattern and porosity levels distribution in the sample volume post-infiltration have been characterized by a high-resolution micro-focus computed tomography (μ CT)

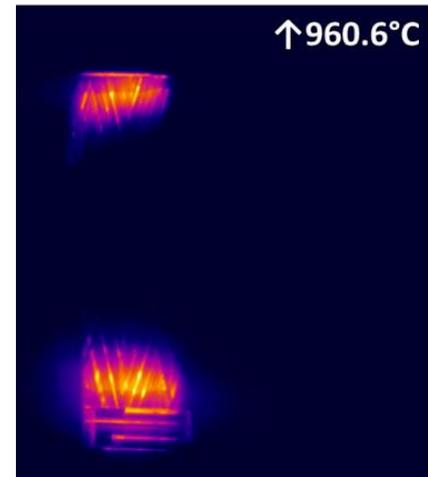


| CT Scan parameters V TOME X M 300 | Square-shaped samples |
|---|-----------------------|
| Voltage/current | 150 kV / 170 μ A |
| Filters | 0.5 mm Cu |
| Focus-to-Object Distance (FOD) - Focus-to-Detector Distance (FDD) | 102.640 - 808.217 mm |
| Voxel size | 26.02 μ m |
| Exposure time | 250 ms |
| Averaging/Skip | 1/0 |
| Sensitivity | 0.5 |

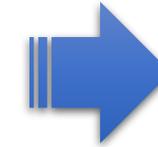
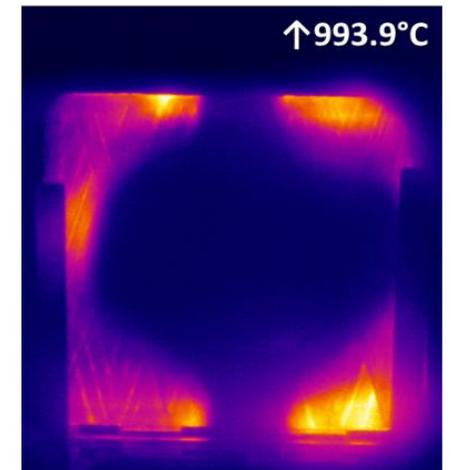
- Both the investigated samples, underwent a 10 h infiltration cycle
- The CMC sample temperature distribution matched quite well with that determined by numerical modelling along WP2 (~5 MHz difference)
- Along the infiltration process, the CMC regions at the infiltration temperature steadily expanded towards the center
- The surface-to-core temperature difference in the CMC sample, estimated by numerical modelling, was of about 80°C

| MW-CVI final Results & Parameters | | | | | | |
|-----------------------------------|------------------|----------------------------------|----------|----------|-------------------------------|---------------------------------|
| Pressure [mbar] | Temperature [°C] | Average MW transmitted Power [W] | | | Average deposition rate [g/h] | Average Chemical Efficiency [%] |
| | | SSG1 | SSG2 | SSG3 | | |
| | | 200 | 900-1000 | 2428 MHz | | |
| | | 473 | 548 | 470 | | |

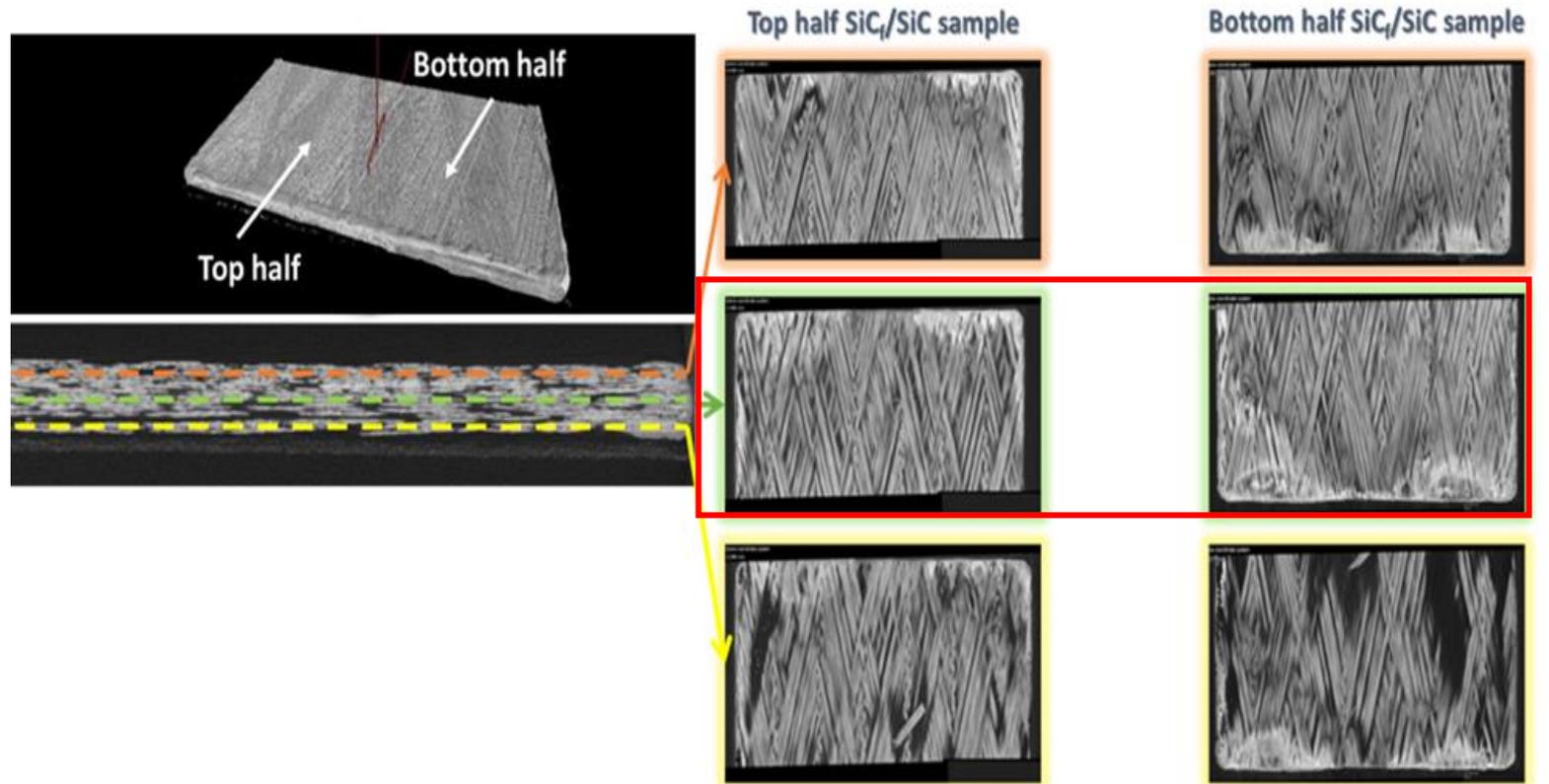
T profile – Infiltration start



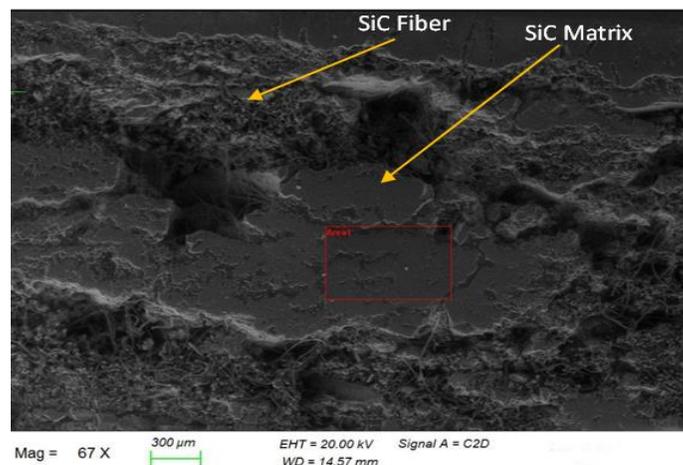
T profile – After 10 h infiltration



❖ The obtained results confirmed the inside-out densification pattern, expected from the sample volumetric heating



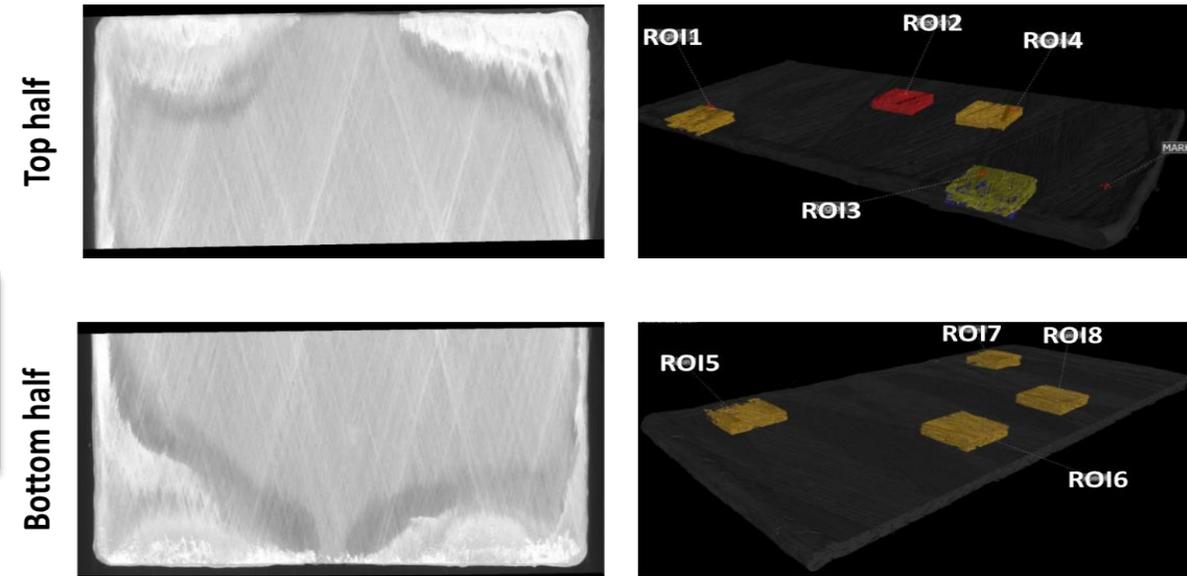
❖ SEM-EDS analysis confirmed the presence of a homogeneous SiC matrix (Si:C ratio of 0.8)



| Element | Atomic No. | Atom Norm. [%] |
|---------|------------|----------------|
| C | 6 | 51.83 |
| O | 8 | 7.5 |
| Si | 14 | 40.67 |

❖ A consistent reduction in porosities across the targeted regions, compared to the starting values, has been observed

▪ The results of these activities have been reported in a recent joint paper on JECS, recently accepted for publication.

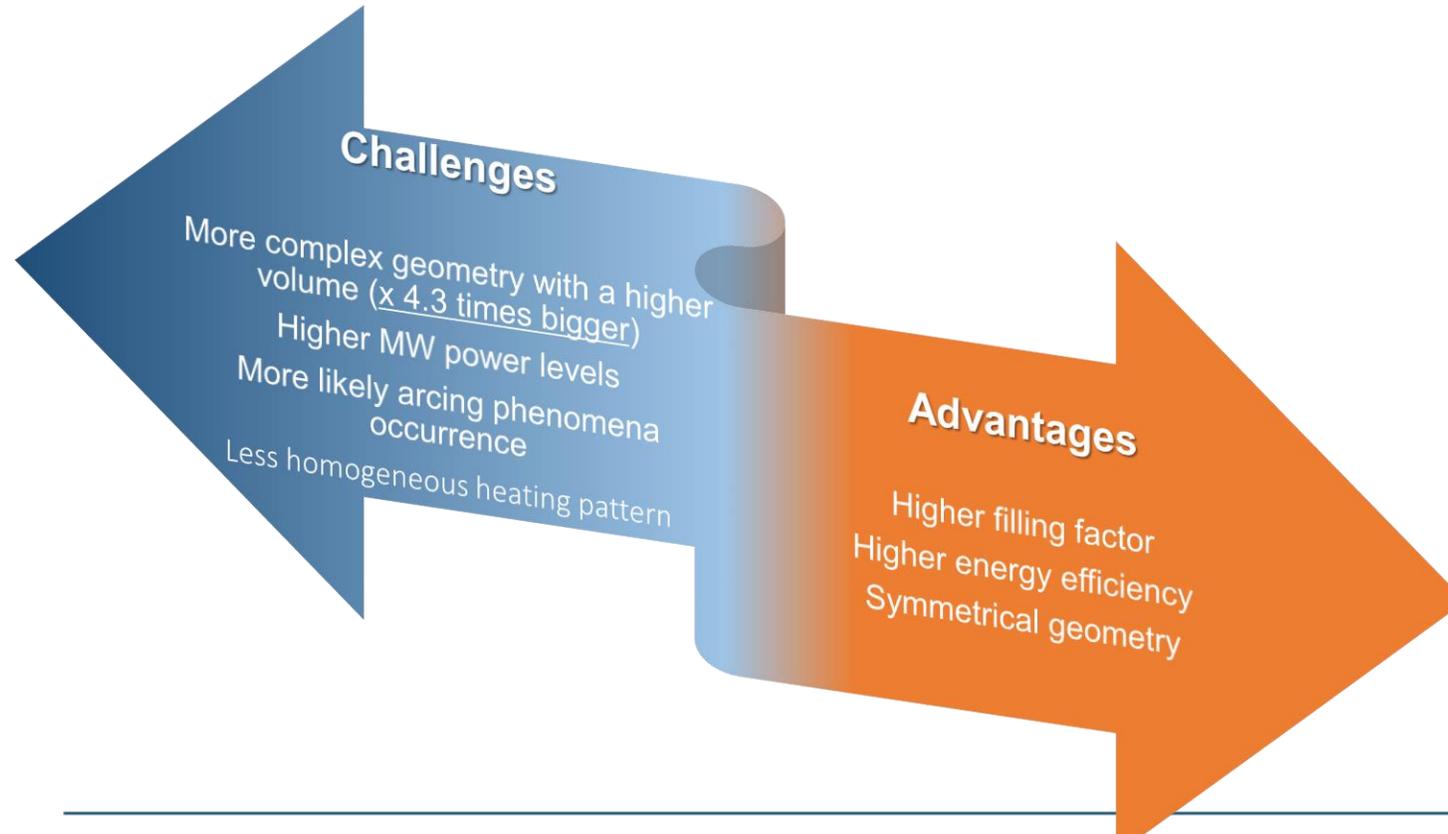


| | Top half SiC _f /SiC sample | | | | Bottom half SiC _f /SiC sample | | | |
|---------------------------|---------------------------------------|-----|-----|-----|--|-----|-----|-----|
| ROI | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Volume [mm ³] | 173 | 161 | 221 | 158 | 223 | 181 | 243 | 165 |
| Porosity [%] | 29 | 39 | 27 | 37 | 15 | 27 | 20 | 31 |

3.1 MW-CVI processing of SiC_f/SiC tubular preforms

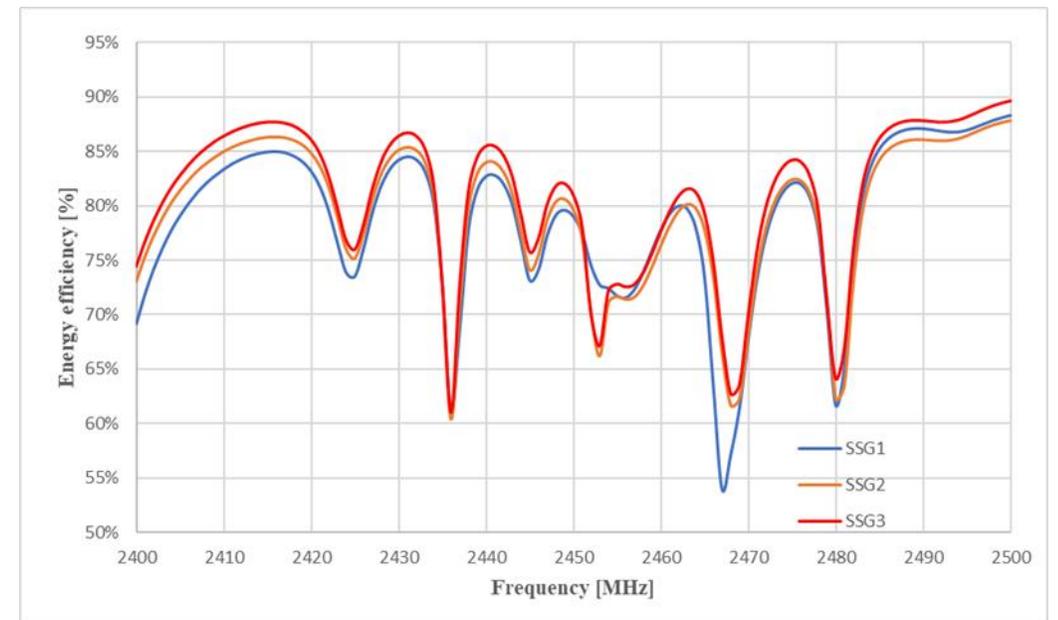
- The selection of the optimal MW heating parameters was guided by the rigorous numerical modelling of the loaded reactor;
- The Multiport-Multifrequency approach has been employed during the MW-CVI trials.

| #ID sample | SiC _f /SiC-C2 |
|------------------------------|--------------------------|
| Roving | 200 tex |
| Green body matrix | Epoxy |
| Pyrolised matrix | Carbon |
| Porosity [%vol] | 50.2 |
| Density [g/cm ³] | 1.42 |
| Geometry [D x L x T, cm] | 10×12.7×0.3 |



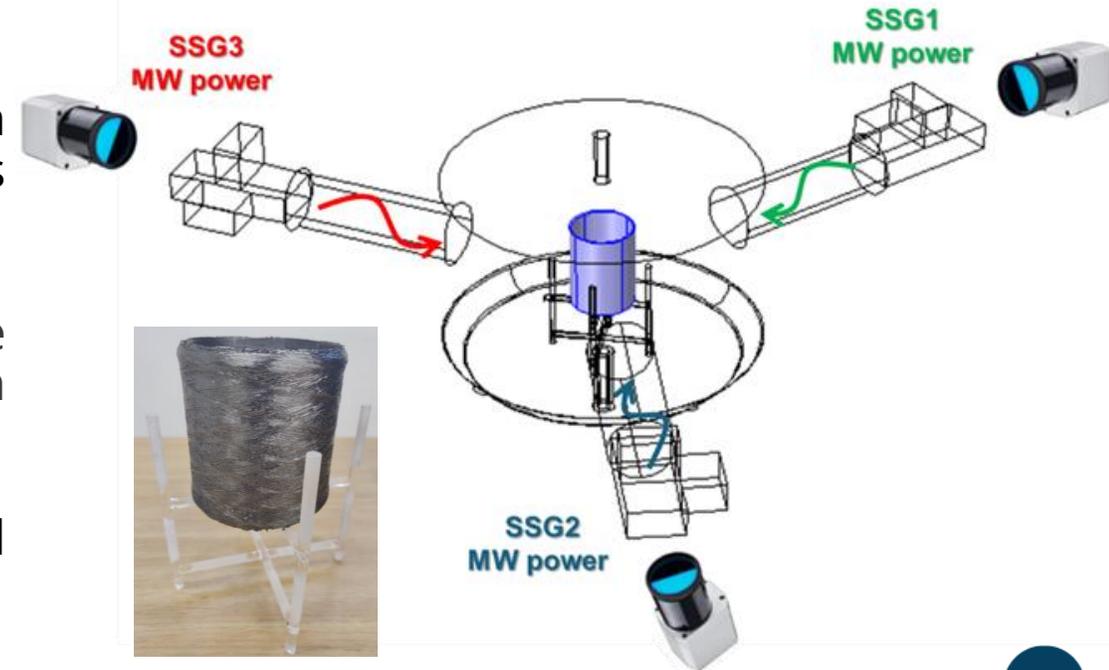
EM assessment of the loaded MW-CVI reactor

- The modes distribution is independent from the excitation port
 - The identification of the optimal operating frequency, in the electromagnetic models, is simplified;
 - More stable behavior in frequency during the MW-CVI process due to the reduced modes density with resonance curves characterized by larger linewidths.



Sample heating configuration selection

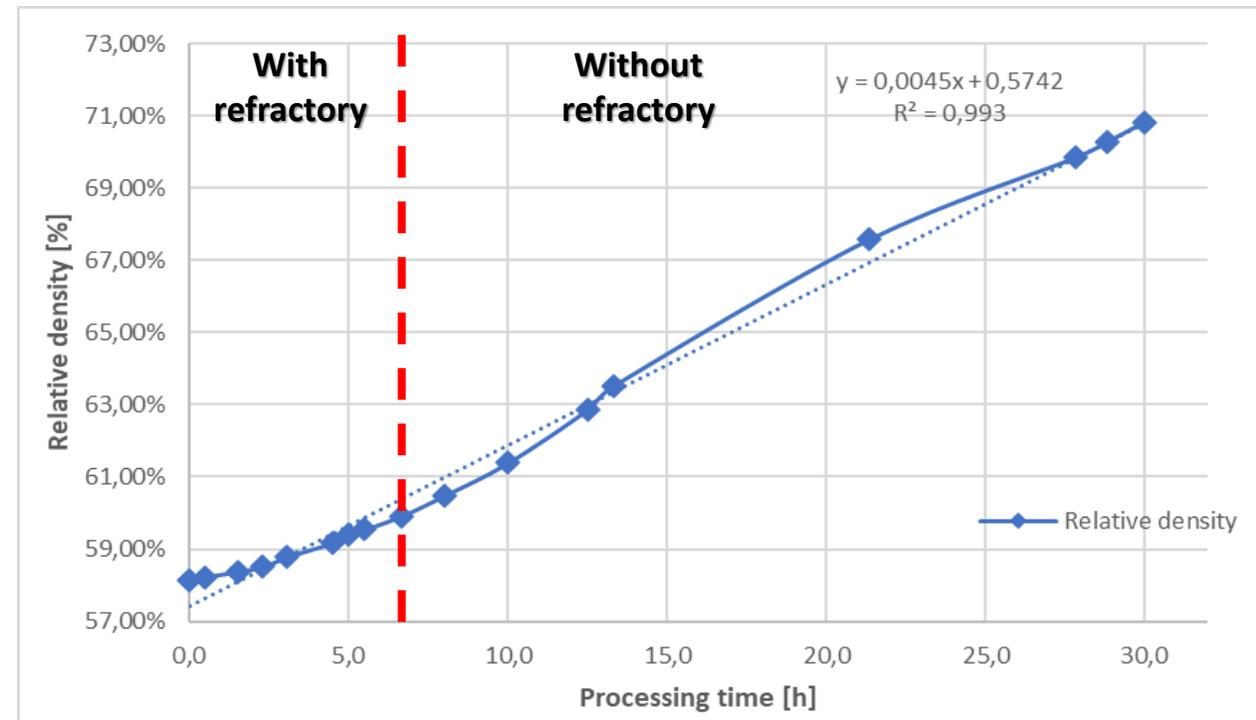
- A temperature monitoring configuration to obtain an almost 360° view of the sample heating pattern has been implemented
 - 75% of the overall $\text{SiC}_f/\text{SiC-C2}$ surface could be monitored with the defined material configuration in the reactor;
 - The heating pattern uniformity has been evaluated by an in-house developed Python code.



- SiC_f/SiC-C2 sample underwent a total of 30 h of MW-CVI processing
 - The MW-CVI reactor proved quite robust in terms of resonance frequency shift with the SiC_f/SiC sample dielectric properties variation during the process;

| MW-CVI tests SiC _f /SiC tube: Average operating parameters | | | | |
|---|------------------|----------------------------------|-------------|-------------|
| Pressure [mbar] | Temperature [°C] | Average MW transmitted Power [W] | | |
| | | SSG1 | SSG2 | SSG3 |
| 200 | 836.6 ± 19.3 | 2480 - 2487 | 2484 - 2487 | 2476 - 2484 |
| | | MHz | MHz | MHz |
| | | 1404 | 1413 | 1270 |

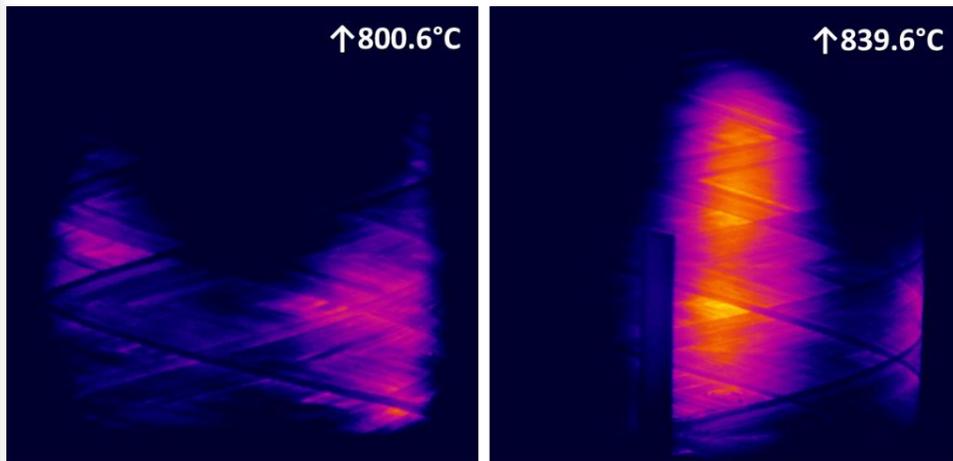
- The relative density increased from 58% to 71% (density 2.4 g/cm³ - residual porosity of 15-20 %vol)
- The densification process has been not straightforward due to:
 - Presence of a 10 %wt C matrix;
 - Presence of the mullite-based refractory.



MW-CVI trials with refractory

- ❑ Tubular-shaped mullite-based refractories have been employed during first MW-CVI trials to:
 - Minimize the MW power requirements while improving the heating pattern uniformity
- ❑ The starting sample temperature distribution was characterized by only small regions at the infiltration temperature

T profile – Infiltration start (Channel 1+2 view)

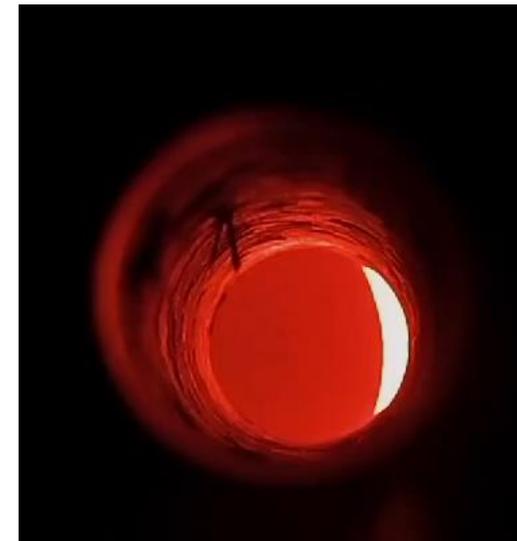


Uniformity ($T_{\text{threshold}} = 800 \text{ }^\circ\text{C}$) = 0 % Uniformity ($T_{\text{threshold}} = 800 \text{ }^\circ\text{C}$) = 0.95 %



| Altraform KVS 184-400 (Rath, Germany) | |
|---------------------------------------|------------------------------------|
| Geometry [D x L, cm] | 8 × 10; 6 × 10 |
| Composition [% wt] | Al ₂ O ₃ 78% |
| | SiO ₂ 22% |
| Max application temperature [°C] | 1800 |
| Density [g/cm ³] | 0.4 |

- ❑ Mullite, as well as other silica (SiO₂) based refractories, reacts with H₂ at temperatures of about 1400°C [1]:



❑ The latter reactor configuration forced us to daily MW-CVI trials with durations among 30 to 90 minutes

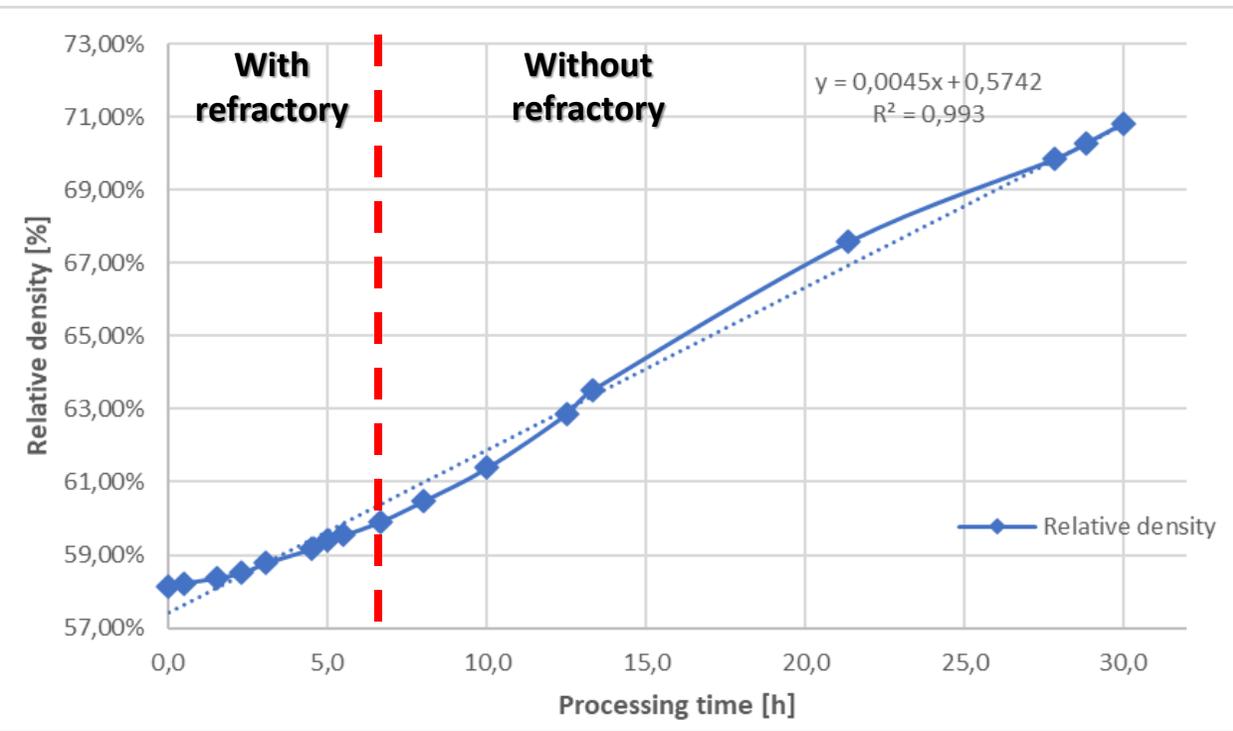
❑ After 6.5 hours of MW-CVI processing, corresponding to the SiC_f/SiC tube weight increase (i.e. SiC matrix increase) of 3.26 g (1.32 %vol)

▪ A comparable heating pattern with respect to the starting point, but without the refractory, has been obtained as a result of the material dielectric properties improvement

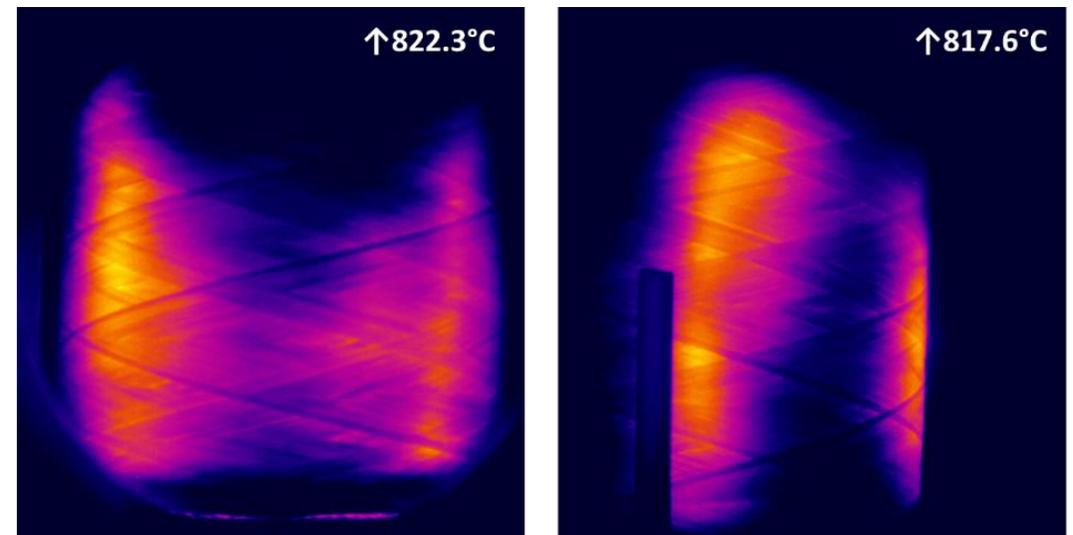
❑ MW-CVI runs of about 8 hours, split among three different days, without the need to open the reactor

▪ Due to the lack of the reactor stainless steel lateral wall water cooling system, we had to limit daily runs to max 3.5 hours;

▪ The possibility of performing 8 hours long continuous process run has been proved.



T profile – After 6.5 h (Channel 1+2 view)

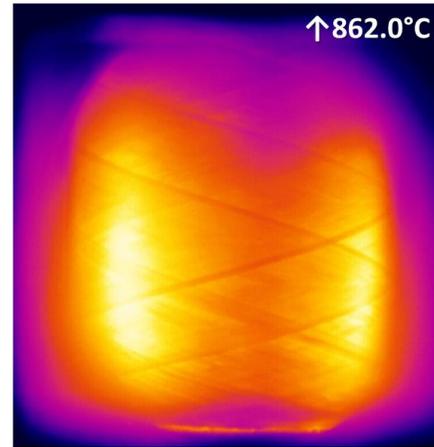


Uniformity ($T_{\text{threshold}} = 800 \text{ }^\circ\text{C}$) = 0.25 %

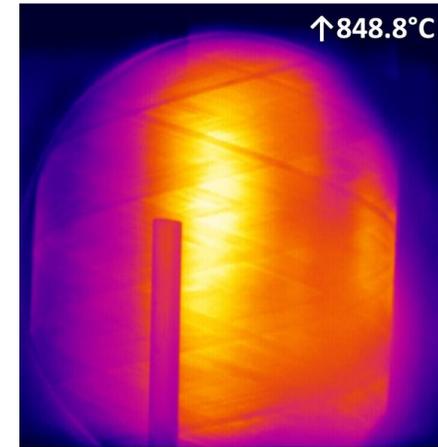
Uniformity ($T_{\text{threshold}} = 800 \text{ }^\circ\text{C}$) = 0.19 %

T profile – After 30 h (Channel 1+2+3 view)

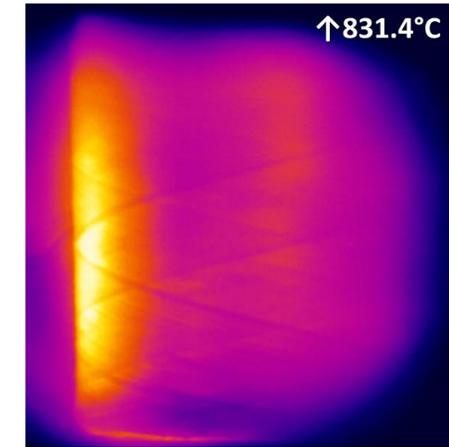
- Longer MW-CVI runs have been realized in the subsequent trials collecting additional 23.5 hours, corresponding to the SiC_f/SiC tube weight increase (i.e. SiC matrix increase) of additional 20.15 g (9.48 %vol)
 - Remarkable increase of the sample heating pattern uniformity



Uniformity ($T_{\text{threshold}} = 800\text{ }^{\circ}\text{C}$) = 15.00 %



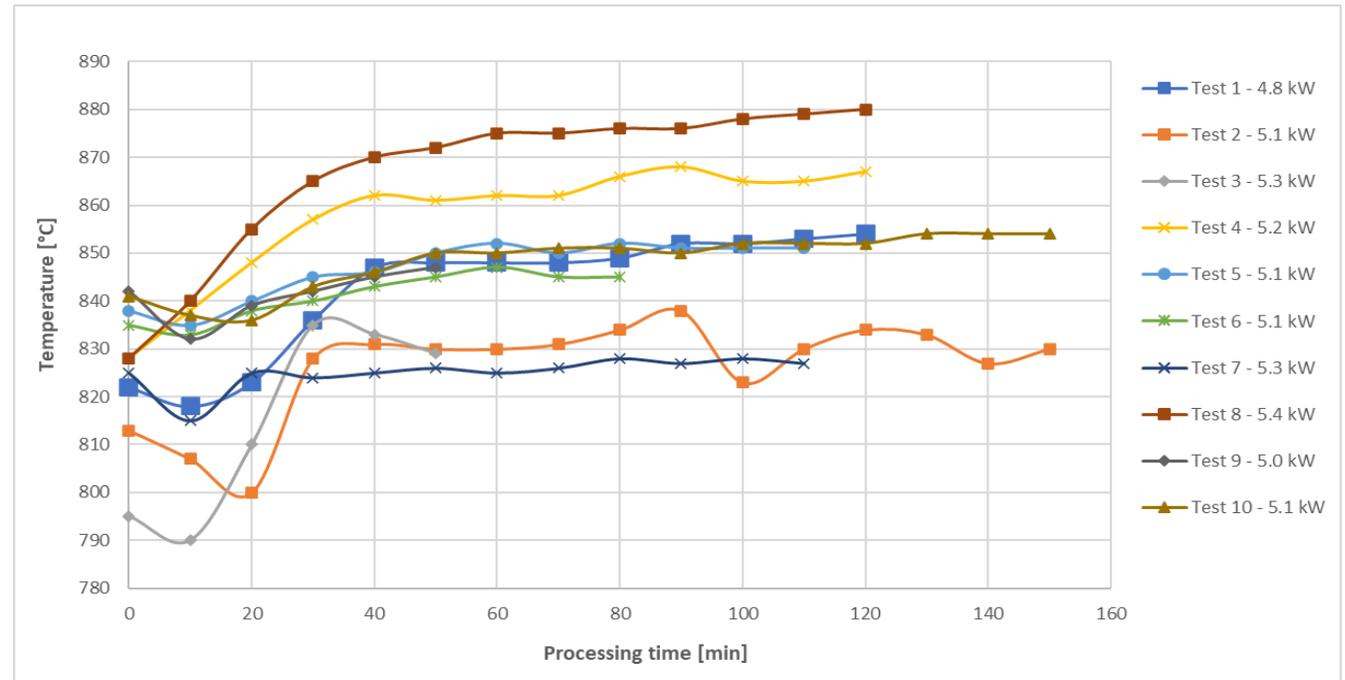
Uniformity ($T_{\text{threshold}} = 800\text{ }^{\circ}\text{C}$) = 9.68 %



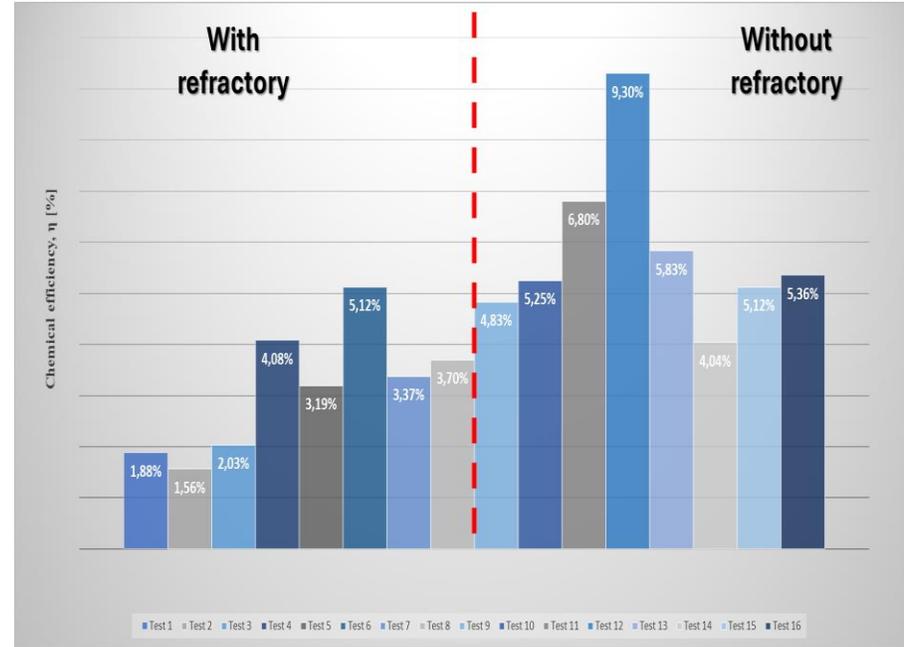
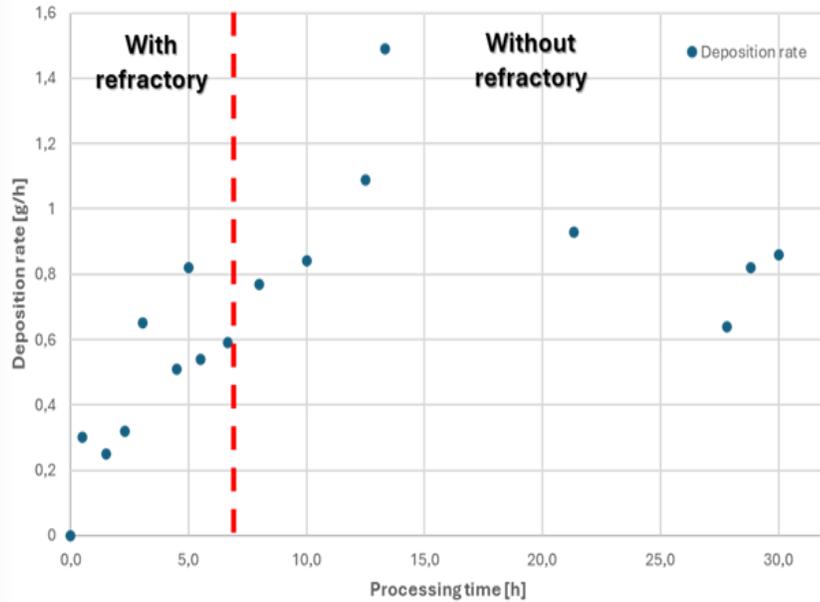
Uniformity ($T_{\text{threshold}} = 800\text{ }^{\circ}\text{C}$) = 3.26 %

- Another point of interest is represented by the temperature evolution during each trial:

- During each test, T increased at constant MW power differently from previous literature studies;



- These results translated in an increase of the SiC matrix deposition rates and thus of the process chemical efficiency (max value of **9.3%** with a deposition rate of **1.5 g/h**)



- An average deposition rate of **0.93 g/h** has been computed without the refractory:

$$t_{miss} = \frac{\Delta M_f}{M_i} * \frac{1}{V_{SiC}} = 51 \text{ h}$$

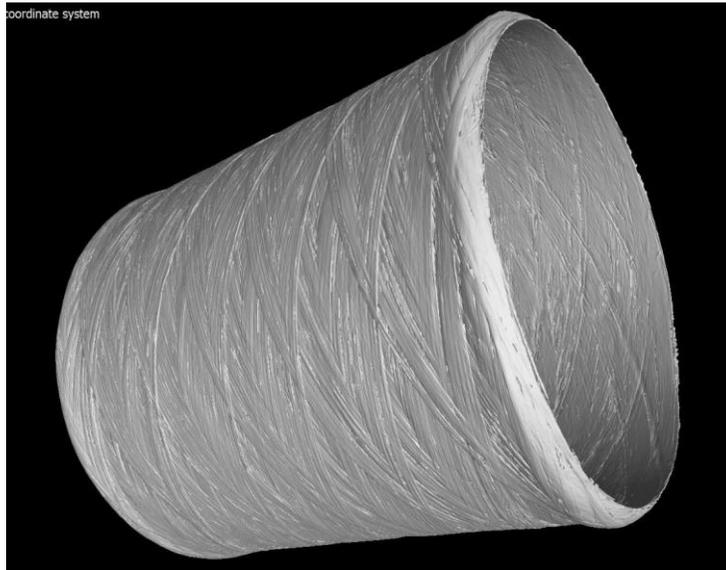
- A total MW-CVI processing time of **81 h** has been estimated!

- The overall SiC_f/SiC-C2 composite components content variation during each stage have been evaluated

- The overall sample porosity had been reduced of about 9.5% in 30 h

| | Start | After MW-CVI processing with Refractory | After MW-CVI processing without Refractory |
|-------------------|--------|---|--|
| SiC fibers [%vol] | 42,20% | 42,20% | 42,20% |
| C matrix [%vol] | 7,61% | 7,61% | 7,61% |
| SiC matrix [%vol] | 0,00% | 1,32% | 9,48% |
| Porosity [%vol] | 50,18% | 48,86% | 40,70% |

- ❑ Finally, the **SiC_f/SiC-C2** sample densification has been evaluated through μ CT analysis
- ❑ Due the more complex geometry and dimensions of the sample, a lower resolution has been reached
 - The porosity values determined from the tomographic scans differed of about 20% with respect to the values experimentally measured.



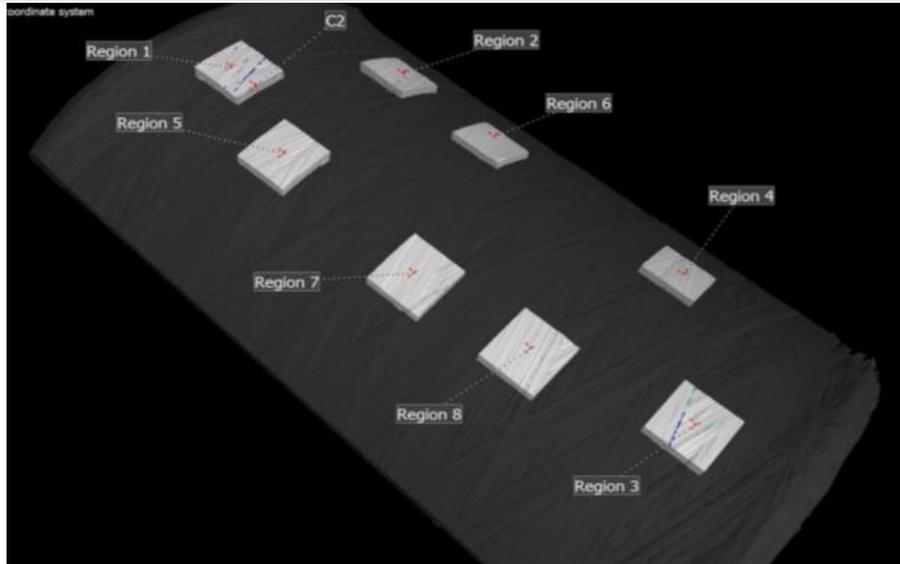
| CT Scan parameters V TOME X M 300 | Tubular-shaped samples |
|---|------------------------|
| Voltage/current | 120 kV / 180 μ A |
| Filters | No filters |
| Focus-to-Object Distance (FOD) - Focus-to-Detector Distance (FDD) | 141.704 - 808.196 mm |
| Voxel size | 35.06 μ m |
| Exposure time | 150 ms |
| Averaging/Skip | 3/1 |
| Sensitivity | 0.5 |

μ CT analysis before MW-CVI trials

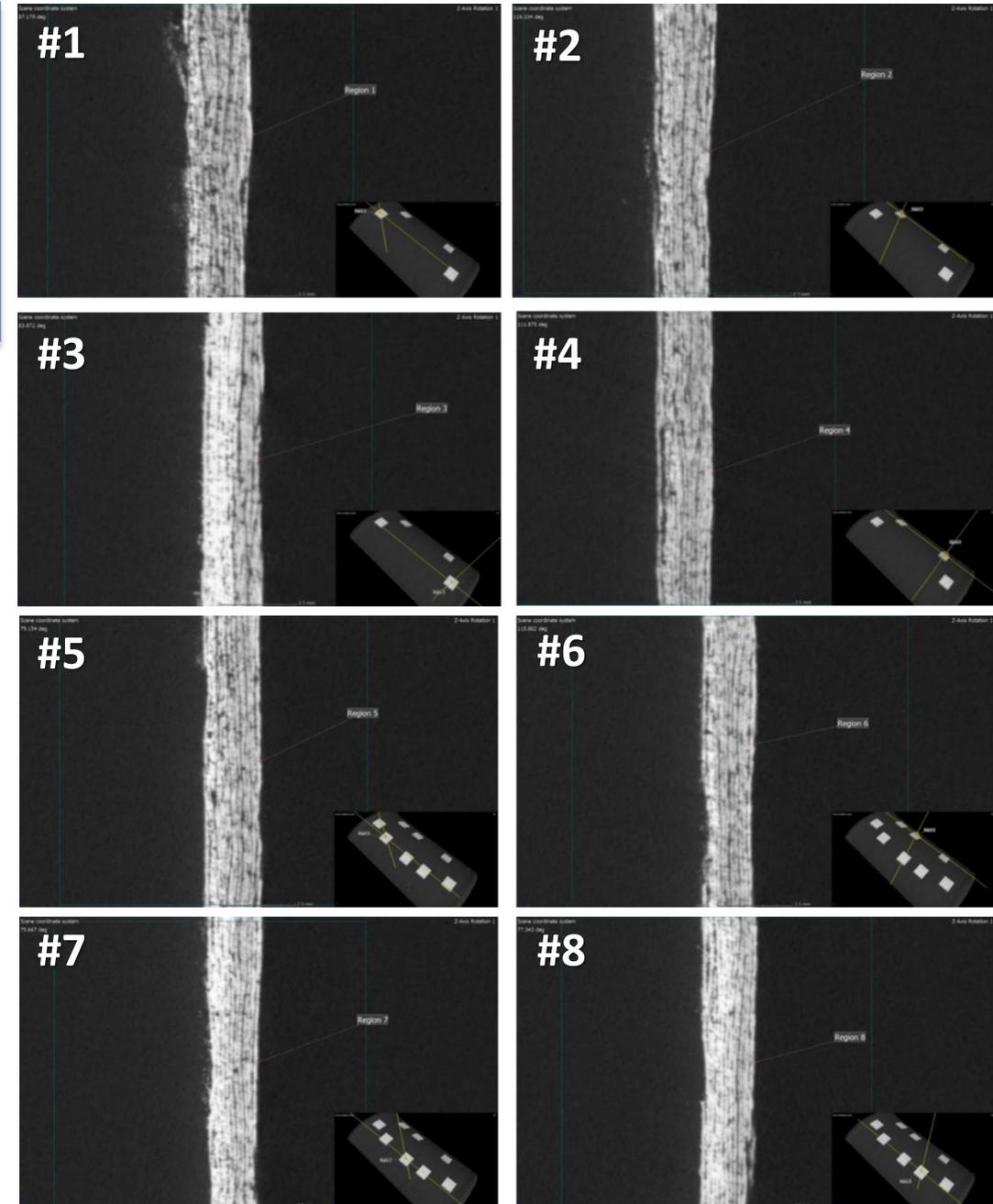


| Area | Porosity [%vol] |
|-----------|-----------------|
| Region #1 | 28 |
| Region #2 | 27 |
| Region #3 | 15 |
| Region #4 | 17 |

- ❑ A homogeneous porosity reduction of about 10 %vol has been observed
- ❑ Most of the regions evidenced a densification front moving from the inner to the outer sample walls (surface-to-core temperature difference of about 30°C)



| Area | Porosity [%vol] |
|-----------|-----------------|
| Region #1 | 11 |
| Region #2 | 15 |
| Region #3 | 10 |
| Region #4 | 19 |
| Region #5 | 9 |
| Region #6 | 7 |
| Region #7 | 6 |
| Region #8 | 6 |



4. Conclusions

- ❖ Both SiC_f/SiC preforms geometries have been successfully infiltrated by MW-CVI process:
 - In the infiltrated regions, a consistent porosity reduction has been observed with values comparable to those obtained by conventional I-CVI;
 - Potential reduction of about one order of magnitude in the processing times;
 - Tailored temperature gradients have been obtained resulting in densification fronts without crusting phenomena;
- ❖ Replacement of the starting C with SiC matrix to obtain more favourable starting dielectric properties
- ❖ The possibility of automatically maximize the heating pattern uniformity will result in significant steps ahead in view of the possible industrial scale-up of the MW-CVI technology



NOVEL CERAMICS AND COMPOSITES PROCESSING TECHNOLOGIES FOR ENERGY-INTENSIVE APPLICATIONS

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THANK YOU



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